

# Estimating SAR polarimetric system errors in the presence of Faraday rotation using a transponder

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# A PARC plays a key role in BIOMASS calibration



Selected site: New Norcia, NSW, Australia

Calibration roles:

- Characterisation of antenna pattern
- Radiometric calibration
- Polarimetric calibration

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# The system model



The basic system equation is:

$$\begin{split} \boldsymbol{M} &= \begin{bmatrix} M_{hh} & M_{vh} \\ M_{hv} & M_{vv} \end{bmatrix} \\ &= A(r,\theta)e^{j\varphi} \begin{bmatrix} 1 & \delta_2 \\ \delta_1 & f_1 \end{bmatrix} \begin{bmatrix} \cos\Omega & \sin\Omega \\ -\sin\Omega & \cos\Omega \end{bmatrix} \begin{bmatrix} S_{hh} & S_{vh} \\ S_{hv} & S_{vv} \end{bmatrix} \begin{bmatrix} \cos\Omega & \sin\Omega \\ -\sin\Omega & \cos\Omega \end{bmatrix} \begin{bmatrix} 1 & \delta_3 \\ \delta_4 & f_2 \end{bmatrix} + \begin{bmatrix} N_{hh} & N_{vh} \\ N_{hv} & N_{vv} \end{bmatrix} \end{split}$$

More compactly, for polarimetric calibration:

M = RFSFT + N (*N* here includes clutter)

With the PARC we can generate a known form of the S matrix. Then, with no noise, on the right we have 13 real unknowns:

- 1 real unknown ( $\Omega$ )
- 6 complex unknowns (the  $\delta_i$  and  $\varepsilon_i$ , where  $f_i = 1 + \varepsilon_i$ )

On the left we have 4 complex (8 real) measurements.



The PARC can simultaneously generate multiple targets with different scattering matrices

$$\mathbf{S}_X = \begin{bmatrix} 0 & 0 \\ 1 & 0 \end{bmatrix} \qquad \mathbf{S}_Y = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \qquad \mathbf{S}_A = \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix} \qquad \mathbf{S}_B = \begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix}$$

Each independent target adds 8 new measurements so we have

• 13 real unknowns and 32 real measurements. Hence many analytic ways to solve the noise-free system (e.g. Chen et al., 2011).

BUT, the PARC is not error-free, so when it tries to produce S, it produces  $S_D$ :

$$\begin{bmatrix} S_{hh} & S_{vh} \\ S_{hv} & S_{vv} \end{bmatrix}_{D} = \begin{bmatrix} 1 & \delta_{T2} \\ \delta_{T1} & f_{T1} \end{bmatrix} \begin{bmatrix} S_{hh} & S_{hv} \\ S_{vh} & S_{vv} \end{bmatrix} \begin{bmatrix} 1 & \delta_{T3} \\ \delta_{T4} & f_{T2} \end{bmatrix} \equiv \mathbf{T}_{P} \mathbf{S} \mathbf{R}_{P}$$

• 6 more complex unknowns, so 25 real unknowns in total.

# With PARC errors we can solve the noise-free system using numerical methods



An analytic solution seems intractable but numerical optimisation can provide an exact solution for:

- the system errors
- the PARC errors
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- 1. What happens when we add clutter + noise?
- 2. Which performs better: the numerical approach or the analytic approach?

To assess this we used simulation:

System & PARC errors & noise were assumed to have:

- zero-mean complex Gaussian distributions
- independent real and imaginary parts with equal variance
- correlations only between  $\delta_1$  and  $\delta_3$ ,  $\delta_2$  and  $\delta_4$ , and  $\varepsilon_1$  and  $\varepsilon_2$ .

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The first step in the Chen analytic solution is estimation of  $\Omega$ . This gives 2 solutions, and the one with the smallest imaginary part is selected.

Mark noticed empirically that we got much better results by averaging the the 2 solutions for  $\Omega$  and taking the real part.

The following results are therefore labelled as

- Chen
- Avg
- Num



## Mean errors as SCNR changes





Mean error in  $\varepsilon_1$ 



Average solution performs much better than Chen. It is almost unaffected by noise. Better than the numerical method except at highest SCNR. Average solution performs better than Chen. It is almost unaffected by noise. Always better than the numerical method.

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# The numerical algorithm may not converge



Test for convergence over 20 different system error realisations as SCNR changes.

100% convergence success only for highest SCNR

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The system we are dealing with is

 $M_i = RFT_p S_i R_P FT + N_i$ 

with i = 1 - 4, so 16 complex measurements. For the unknowns we have

- 6 complex system errors
- 6 complex PARC errors
- 16 complex noise terms
- 1 real Faraday rotation angle.

This looks analytically intractable

## BUT

a 1<sup>st</sup> order analysis of the Average scheme is possible, if all 2<sup>nd</sup> order terms are neglected (i.e. all products of errors, such as  $\delta_1 \delta_3$ ).

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The estimate of  $\Omega$  is **unbiased** with variance

$$V_{\widehat{\Omega}_A} = \frac{1}{4} V_{\delta} (1 - Re[\rho]) + \frac{\langle S^2 \rangle}{16} V_{\varepsilon T} + \frac{1 + \langle C^2 \rangle}{8} V_{\delta T} + \frac{V_N}{4}$$

The estimates of  $f_i$  are both **unbiased** with variance

$$V(\hat{f}) = \frac{1 + \langle C^2 \rangle}{2} V_{\varepsilon T} + \langle S^2 \rangle V_{\delta T} + V_N$$

Their real and imaginary parts both have variance equal to half this value.

The estimates of the imaginary parts of  $\delta_i$  are all **unbiased** with variance  $V\left(Im(\hat{\delta}_i)\right) = \frac{\langle S^2 \rangle}{8} V_{\epsilon T} + \frac{1 + \langle C^2 \rangle}{4} V_{\delta T} + \frac{V_N}{2}$ 

- $C = \cos 2\Omega$  and  $S = \sin 2\Omega$
- $\delta_2$  and  $\delta_4$  have complex correlation coefficient  $\rho$
- T indicates "transponder"

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# 1<sup>st</sup> order analysis: $Re(\hat{\delta}_i)$ is biased, i = 2,4, unbiased i = 1,3 • eesa

The estimates of the real part of  $\delta_1$  and  $\delta_3$  are **unbiased** with variance  $V\left(Re(\hat{\delta}_i)\right) = \frac{1}{4}(1 - Re[\rho])V_{\delta} + \frac{5}{16}\langle S^2 \rangle V_{\varepsilon T} + \frac{1}{8}\langle 1 + 5C^2 \rangle V_{\delta T} + \frac{3}{4}V_N$ 

The estimates of the real parts of  $\delta_2$  and  $\delta_4$  are biased with mean values  $\langle Re(\hat{\delta}_2) \rangle \sim = \frac{1}{2} Re(\delta_2[1 + \rho^*])$   $\langle Re(\hat{\delta}_4) \rangle \sim = \frac{1}{2} Re(\delta_4[1 + \rho])$ The bias gets smaller as  $\rho \to 1$  (if real).

Both have the same variance

$$V\left(Re\left(\hat{\delta}_{i}\right)\right) = \frac{1-|\rho|^{2}}{8}V_{\delta} + \frac{\langle S^{2}\rangle}{16}V_{\varepsilon T} + \frac{\langle 1+C^{2}\rangle}{8}V_{\delta T} + \frac{1}{4}V_{N}$$

For system error variances typical of those expected for BIOMASS, the noise variance is much smaller than the other terms.

The average solution is almost unaffected by clutter + noise.

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# Histograms of estimates of $Im(\delta_i)$ using full simulation



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# Histograms of estimates of $Re(\hat{\delta}_i)$ using full simulation





# **Key conclusions**



- 1. The performance of analytic methods to solve the PARC system for system errors and Faraday rotation is comparable to or better than numerical optimisation.
- 2. Numerical methods may not converge.
- 3. First order analysis indicates biases in the estimates of 2 of the cross-talk terms.
- 4. Correcting this bias should reduce the errors in the cross-talk terms: this analysis still needs to be performed.



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# **Simulation parameters**



Values used for the plots:

- $V_{\delta} = -31 \text{ dB}$
- $V_{\varepsilon} = -25 \text{ dB}$
- $V_{\delta T} = -35 \text{ dB}$
- $V_{\varepsilon T} = -35 \text{ dB}$
- $V_N = -50 \text{ dB}$
- $\rho=0.9~{\rm and}~0.5$

 $\Omega$  is normally distributed with mean 30° and standard deviation 10°.

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For simplicity, we assume that

- the system cross-talk errors (i.e. the  $\delta_i$ ) all have variance  $V_{\delta}$
- the system channel imbalance errors (i.e. the  $\varepsilon_i$ ) all have variance  $V_{\varepsilon}$
- $\delta_2$  and  $\delta_4$  have complex correlation coefficient  $\rho$
- the PARC cross-talk errors (i.e. the  $\delta_{Ti}$ ) all have variance  $V_{\delta T}$
- the PARC channel imbalance errors (i.e. the  $\varepsilon_{Ti}$ ) all have variance  $V_{\varepsilon T}$
- the noise terms all have variance  $V_N$
- $\Omega$  is a random variable;  $C = \cos 2\Omega$ ;  $S = \sin 2\Omega$